

Degradation of concentrating solar thermal reflectors in acid rain atmospheres

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Abstract

Given the importance that concentrating solar power technologies have had in recent years, the interaction between humid atmospheres in which SO₂ is the main pollutant and the metal reflecting layers of the solar concentrators is a major concern that should be addressed. Previous durability studies have urged the importance of designing an accelerated aging test protocol for simulating aggressive industrial atmospheres that solar reflector materials are bound to encounter. Therefore, three types of reflectors were tested in an acid-rain (or Kesternich) chamber at various temperatures and gas concentrations based on the DIN 50018 and ISO 6988 standards. The results showed the significant effect of high SO₂ concentrations rather than high temperatures on silvered-glass reflectors, although synergy should not be disregarded. Strong reductions in specular reflectance were found for one type of silvered reflector compared to another type, highlighting the significance of material processing and its effects on their final performance. Aluminum reflectors were not damaged as much as silvered-glass reflectors, but under microscopic inspection, a wide range of noticeable corrosion defects could be found in all the materials. Comparisons between the most representative Kesternich test and samples from an outdoor industrial site permitted realistic lifetime correlations for commercial silvered-glass reflectors.

Keywords: concentrating solar technology; solar reflector; accelerated aging test; acid rain; service lifetime prediction.

Nomenclature

Acronyms

CSP	Concentrating solar power
PVD	Physical vapor deposition
CASS	Copper-accelerated acetic acid salt spray

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DIN	Deutsches Institut für Normung (German Institute for Standardization)
ISO	International Organization for Standardization
PTC	parabolic-trough collector
ASTM	American Society for Testing and Materials
SLR	Single-lens reflex

Symbols

T	Temperature, °C
RH	Relative humidity, %
V	Volume, dm ³
$\rho_{\lambda,\varphi}(660nm, 15^\circ, 12.5mrad)$	Monochromatic specular reflectance at wavelength $\lambda=660nm$, incidence angle $\theta_i=15^\circ$ and acceptance half-angle $\varphi=12.5 mrad$, -
$\rho_{s,h}([280,2500]nm, 8^\circ, h)$	Solar-weighted hemispherical reflectance in the wavelength range of $\lambda=[280,2500]nm$ and at incidence angle $\theta_i=8^\circ$, -
N	Number of corrosion spots, -
W	Scratch width, μm
$[SO_2]$	Sulfur dioxide concentration, ppm

1. Introduction

Concentrating solar thermal technologies (known as CSP, concentrating solar power) have undergone spectacular development in the last few decades [1]. While in 2006 CSP installed capacity was 0.5 GW_e worldwide, it has increased by a factor of 10 to over 5 GW_e today. It is estimated that CSP technologies will provide about 11% of total electricity production by 2050 [2], as a result of the huge effort made by numerous countries in the last few years in introducing noteworthy renewable-energy programs [3, 4]. CSP plants may be located near industrial areas because of the availability of highly qualified personnel and infrastructures already in place there. In addition, industry is showing growing interest in the use of CSP technologies as the source of electricity, steam and process heat. However, these areas may face significant concentrations of sulfur dioxide (SO₂), which is the gas mainly responsible for atmospheric acidification [5]. This phenomenon, which has been of great concern in the last several years, has resulted in numerous studies [6-8]. Combustion of fossil fuels containing sulfur and smelting metal sulfide ores are the main sources of manmade emissions of SO₂ [9]. Although recent studies have reported a dramatic decrease in atmospheric SO₂ levels in several European cities, mainly due to the use of cleaner fuels and higher-efficiency engines [10], this airborne pollutant (alone or in combination with other corrosive gases and salinity) can cause

serious degradation of metals [11] and in this case, of the metal CSP absorber and reflector parts used in CSP and solar thermal collector applications [12].

Of the current types of CSP reflectors, silvered-glass and aluminum reflectors are the most widely deployed, and both contain metals prone to corrosion, thus negatively affecting their optical performance. Silvered-glass reflectors are based on a thin silver reflective layer which is protected by a 1-4 mm glass substrate on the front and usually a copper layer and several protective coats of paint on the back. Due to their high performance and durability, they have been regarded as the most reliable technology to date [13]. On the other hand, aluminum reflectors consist of a physical vapor deposited (PVD) aluminum layer, on an aluminum substrate protected by transparent SiO_2 sol-gel coatings. They are frequently used in small-scale concentrators for process heat applications where atmospheres are likely to be polluted [14].

The importance of the interaction between gases in ambient air and the silver used in solar concentrator reflectors was identified by Schissel and Czanderna in 1980 [15]. As reported in previous studies [16, 17], humid atmospheres in which SO_2 is the main corrosion agent are aggressive and harmful to many metals (silver, copper, etc.), which are also present in the reflective layer of solar reflectors, thus compromising their optimal performance. More recent studies have carried out extensive laboratory and outdoor exposure testing of solar reflector materials. The most appropriate accelerated aging test that reproduced similar degradation to outdoor defects in silvered-glass reflectors was reported to be the copper accelerated salt spray (CASS) test [18, 19]. Nevertheless, an additional accelerated aging test campaign simulating aggressive industrial environments was considered necessary. A wide variety of accelerated aging experiments have been applied to aluminum reflectors and some correlations with representative outdoor sites derived [20]. One type of corrosion mechanism reproduced with the CASS test and acceleration factors for three different types of reference sites have been assigned accordingly. However, this is only a first step in lifetime prediction of solar reflector materials. To date, few solar reflector durability studies have succeeded in providing realistic lifetime estimates [21], and only a few of them have been devoted to the effect of humid sulfur-containing atmospheres [5, 22, 23]. It is therefore considered a major issue that must be addressed and studied carefully. Special attention should be given the Kesternich test [24, 25], which uses high concentrations of SO_2 in water-saturated atmospheres and has been used before to simulate the degradation of materials normally subjected to atmospheric SO_2 . This standardized aging experiment has been used, for example, to study the degradation and corrosion of historical stained glass windows [26], Zn protective coatings used in medical equipment [27] and the suitability and durability of an anti-graffiti product for porous materials in monuments and historic buildings [28]. Nevertheless, there are various procedures for studying the many types of solar reflector degradation, mainly focused on the effects of erosion [29] and corrosion [30].

In view of the significant corrosion of the metals in solar reflectors by atmospheric SO_2 , the aims of this study were to:

- Examine the behavior of three different types of conventional solar reflectors subjected to a number of accelerated aging tests based on the current Kesternich test methods. Several scenarios were explored, including different temperatures and corrosive gas concentrations at 100% relative humidity.
- Select the most suitable accelerated-aging conditions for solar reflector applications and the best reflector material for high-humidity SO_2 -containing atmospheres.

- Compare accelerated aging results with exposure to outdoor industrial environments of industrial interest and establish preliminary correlations between them.

To approach these objectives, three reflector materials were weathered in eight different corrosion tests with a wide range of ambient conditions and several evaluation methods were used to assess their performance. Finally, the acceleration factor in one of the aging experiments was calculated by comparing it to one real outdoor exposure.

2. Material and methods

This section includes a description of the reflector materials studied, the aging tests carried out and the evaluation techniques used to characterize their degradation.

2.1. Reflector materials

Three candidate commercial solar reflectors were selected for the corrosion experiments, two second-surface silvered-glass reflectors (Types 1 and 2) and a first-surface aluminum reflector (Type 3), as described in [31]. Fig. 1 shows a 10x10 cm² sample of each glass reflector and a 12x12 cm² sample of the aluminum reflectors. Three replicates were used to ensure representative results of corrosion tests. Type 1 silvered-glass reflector samples were cut from larger commercial parabolic-trough collector (PTC) mirror facets having unprotected edges. The samples were also scratched so that all the protective and reflective layers were penetrated, exposing the metal directly to the corrosive atmosphere. The scratch has already been used in the literature [31] to represent damage that reflectors may already have undergone at a real site due to aggressive external conditions, such as sandstorms [32], careless handling, cleaning procedures [33], etc.

As seen in Fig. 1left, Type 1 silvered-glass samples are the most unfavorable case of silver exposed to the corrosive environment, because all three have unprotected cut edges and a 2-cm-long scratch in the paint on the back. In contrast, the silver in Type 2 silvered-glass reflectors (Fig. 1center) is less exposed, since they were specifically manufactured to a 10x10 cm² format specification with four original, protected edges and no deliberate damage. Therefore, Type 1 reflectors are referred to as predamaged silvered-glass reflectors and Type 2 as undamaged silvered-glass reflectors. Both Type 1 and Type 2 samples were produced by the same commercial silvered-glass reflector manufacturer. Edges are not protected in aluminum reflectors for real applications, and so first-surface aluminum reflectors (Fig. 1right) include both unprotected edges and a 2-cm scratch on the front, to expose the reflective layer to the corrosive atmosphere. The main features of the reflector materials studied are summarized in Table 1.

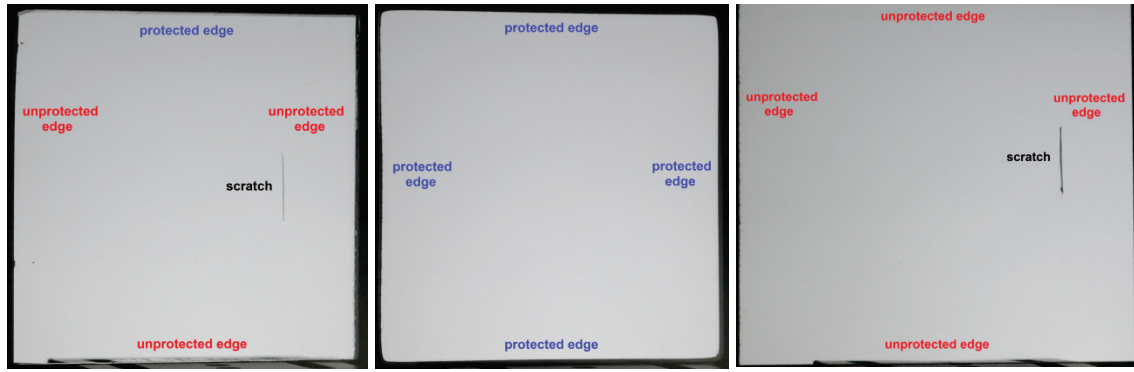


Fig. 1. Solar reflector samples weathered in the corrosion experiments: Type 1, predamaged silvered-glass reflector (left), Type 2, undamaged silvered-glass reflector (center), and Type 3, predamaged aluminum reflector (right). The protected edges are marked in blue, unprotected edges in red and the scratch in black.

Table 1. Main characteristics of solar reflector materials.

Features	Type 1 silvered-glass	Type 2 silvered-glass	Aluminum
Type of reflector	Second surface	Second surface	First surface
Main use	Heliostats/PTC	Heliostats/PTC	Small concentrators
Size (cm ²)	10x10	10x10	12x12
Material layers	Low iron glass/Ag/Cu/Paint coatings	Low iron glass/Ag/Cu/Paint coatings	Nano-composite/PVD layer system/Anodizing layer/Al substrate
Typical initial $\rho_{\lambda,\varphi}(660nm, 15^\circ, 12.5m rad)$	0.950±0.001	0.959±0.001	0.828±0.001
Type of edge protection	1 original edge + 3 fractured edges	4 protected edges	4 unprotected edges
Scratch	Yes	No	Yes

2.2. Weathering experiments

An HK 300 M weathering chamber, also known as a Kesternich cabinet (Fig. 2left), was used for the corrosion experiments (Kesternich tests) following the ISO 6988 and DIN 50018 standards [24, 25]. The test temperature, T , may be varied from +5 °C to +50 °C and the SO₂ doses from 0.1 to 6.0 dm³ (333.3-20000 ppm). Three Kesternich tests at 0.2, 1.0 and 2.0 dm³ of SO₂ in a 300 dm³ chamber interior were performed as proposed in the aforementioned standards. The tests consist of 24-hour cycles divided into two phases. The first one is the heating-corrosive phase, in which the samples are exposed for 8 h to condensed humidity ($RH=100\%$) at 40 °C and the targeted SO₂ concentration. In the second phase, for the following 16 h, the samples are subjected to ambient conditions, i.e. no gas, room temperature (18-28 °C) and $RH=75\%$ maximum. To study the influence of temperature, two additional tests were carried out at 25 and 50 °C and the SO₂ dose set at 1.0 dm³. This volume was considered the most appropriate of the three, because degradation was more significant than at the low concentration, but not as extreme as at the high concentration (see section 3). Finally, the same cyclic weathering experiments were reproduced without gas at the same RH and T (25, 40 and

50 °C) using a standard climatic chamber (Fig. 2right) in order to study the difference between degradation with and without SO₂.

To summarize, the experimental conditions of the eight weathering tests performed in this study are presented in detail in Table 2. The SO₂ volume (in dm³) and temperature (in °C) are given in the test name to distinguish between the different experimental conditions, e.g., K_1_40 stands for the Kesternich test at $V_{SO_2}=1$ dm³ and $T=40$ °C. All the tests consisted of a total of 20 cycles, and samples were analyzed before the tests and after 1, 2, 5, 10, 15, and 20 cycles, as recommended by the DIN 50018 standard. Samples were placed inside the chambers on a tray made of an inert material at a 45° tilt angle. They were gently rinsed with deionized water before optical analysis.

Table 2. Corrosion test conditions.

Name of test	V_{SO_2} (dm ³)	[SO ₂] (ppm)	T (°C)	RH (%)
K_0_25	0.0	0.0	25	100
K_0_40	0.0	0.0	40	100
K_0_50	0.0	0.0	50	100
K_0.2_40	0.2	666.7	40	100
K_1_25	1.0	3333.3	25	100
K_1_40	1.0	3333.3	40	100
K_1_50	1.0	3333.3	50	100
K_2_40	2.0	6666.7	40	100



Fig. 2. Kesternich test chamber HK 300 M KÖHLER Automobiltechnik GmbH (left) and Vötsch condensed water test chamber (right).

2.3. Reflector assessment

Monochromatic specular reflectance, $\rho_{\lambda,\phi}(660\text{nm}, 15^\circ, 12.5\text{mrad})$, was monitored at a 15° incidence angle in a wavelength range of 635 to 685 nm with a peak at 660 nm, and 12.5 mrad acceptance angle with a portable Devices and Services 15R-USB reflectometer [34]. Nine different areas were measured in every reflector sample, with three repetitions in the area of the scratch, for statistically representative results as described in the literature [31].

Spectral hemispherical reflectance, $\rho_{s,h}([280,2500]\text{nm}, 8^\circ, h)$, was determined from 280 to 2500 nm at an 8° angle of incidence using a Perkin Elmer Lambda 1050 spectrophotometer with a 150 mm diameter integrating sphere accessory [35]. Solar-weighted hemispherical reflectance was calculated following ISO Standard 9050 [36] and the direct solar radiation spectrum from ASTM G173-03 [37]. Due to equipment restraints, hemispherical reflectance was only measured at the reflector center, but every sample was measured three times, rotating 90° each time to check for any possible anisotropy.

As previously demonstrated [31], reflectance does not always give enough information to thoroughly assess the performance of solar reflectors. Therefore, several different microscopic and analytical techniques were used to characterize the corrosion defects of greatest interest. Visual characterization was performed with a Panasonic LUMIX model DMC-F745 digital camera. Microscopic defects on the reflective layer and painted side of the silvered-glass reflectors and on the reflective surface of the aluminum reflectors were inspected by optical microscopy using a Zeiss Axio CSM 700 3D light confocal microscope [38], which can work in both 2D optical and 3D confocal modes. Damage was also measured with this microscope, taking into account that the maximum dimension of corrosion spots is their characteristic length. The reflector surface was also evaluated with an in-house device which takes single-lens reflex (SLR) images of the specimens in a dark chamber, and then the corrosion spots and total corroded area were assessed using a MATLAB routine. Means of total corroded areas were given for every three replicates tested per reflector type.

3. Results and discussion

This section presents and discusses the most significant results of the three reflector types studied. It also compares the results of one of the accelerated tests to corrosion data from one exposed near a real industrial site and a correlation is made.

3.1. Predamaged silvered-glass reflectors (Type 1)

Reflectance is the best parameter for quantifying the optical quality of solar reflectors [39]. Consequently, both monochromatic specular and hemispherical reflectance were monitored during the tests. The results of the reflective area undamaged at the start of the experiment (i.e. all of the reflector surface except the area of the scratch [31]) are shown in Fig. 3. No significant changes were observed in the specular reflectance measured. Although a loss of -0.002 ± 0.002 was found at the end of the tests at the highest temperature (K_0_50 and K_1_50, shown in Fig. 3left), it is considered negligible, because it is within the measurement uncertainty of the equipment. Results were similar for the decrease in solar-weighted hemispherical reflectance, as displayed in Fig. 3right.

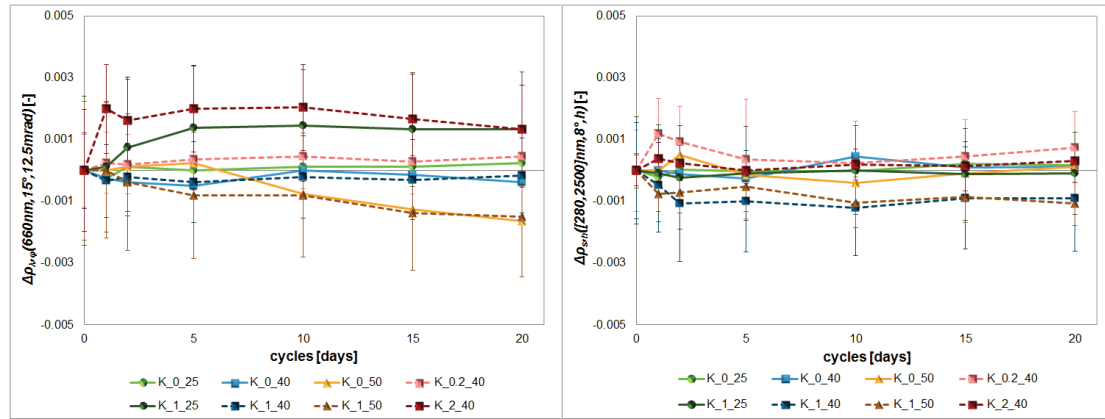


Fig. 3. Changes in mean increment in monochromatic specular reflectance during cycles (left) and in solar-weighted hemispherical reflectance (right) in the undamaged areas of Type 1 silvered-glass reflectors in weathering tests.

The reflectance results show that reflector surfaces were apparently not degraded by the Kesternich tests. But as already reported in previous studies [31], it is very important to analyze the optical performance of reflectors further with other tools. The samples were therefore also examined by optical microscopy on both the reflective surface and painted back to track the appearance and development of any defects. Table 3 summarizes the most significant corrosion defects found on the reflective layer of Type 1 silvered-glass reflectors at the end of testing (20 cycles). According to these microscopic results, the damage done in the SO₂-free tests was negligible, while the tests with the gas may be classified by severity as low (K_0_2_40), medium (K_1_25, K_1_40) and high (K_1_50, K_2_40) as follows.

K_0_2_40 is considered to be a low severity test because it produced only a few (6) small spots on the reflector surface, no corrosion of the original (protected) sample edges, and cut (unprotected) edges were only moderately affected. In addition, corrosion of the total reflector area (Total Corr. in Table 3) was (1.8±0.5)%. Both K_1_25 and K_1_40 are classified as medium, with a total corrosion area of (2.6±0.4)% and (3.7±1.1)%, respectively. However, there are some differences between them. Whereas K_1_40 caused more corrosion near the edges than K_1_25 (218 and 82 μm larger on cut and original edges, respectively), corrosion spots were larger in the latter (the largest spot found was 109 μm larger in K_1_25).

Tests K_1_50 and K_2_40 were responsible for the worst reflector degradation, (5.6±1.0)% and (11.5±1.6)% of the total corroded area, respectively. Numerous large spots also appeared under the extreme conditions (up to 95 spots with a maximum characteristic length over 1100 μm), as well as significant corrosion penetration near the edges, which is even visible to the naked eye after Test K_2_40 (up to centimeters long). Therefore, Test K_2_40 is more aggressive than K_1_50, suggesting that higher gas concentration is more harmful than higher *T*, although synergy of both parameters should also be considered.

Although the tests with no gas (K_0_25, K_0_40 and K_0_50) did not cause any significant degradation on the reflective layer of Type 1 reflector materials, these humidity tests do promote occasional blistering of the paint on the back, as shown in Fig. 4. Such blisters might not be easy to detect in the gas tests because they are prone to flaking off and leaving pinholes as a result of the high severity of the Kesternich tests [40]. Even though not all corrosion spots

may have a corresponding pinhole in the paint, the presence of such a pinhole probably promotes the formation of a corrosion spot. Table 4 shows examples of correspondence between corrosion spots on the reflective layer and pinholes found on the back coating of reflector materials after aging with Kesternich tests.

Table 3

Summary of corrosion found on the reflective area of Type 1 silvered-glass reflectors after 20 cycles of all weathering tests. Total N : sum of the number of corrosion spots visible to the naked eye at the end of testing on a 300-cm² total reflector surface, Size: characteristic length of the largest spot (μm), Max. Pen.: maximum penetration of corrosion near the edge (μm), $\Delta\rho_{\lambda,\varphi}$: mean increment in monochromatic specular reflectance on reflector surfaces not predamaged (-), Total Corr.: mean total corrosion of the whole reflector surface (%). Microscope images are 10x.

Corrosion features		Reflective area of Type 1 silvered-glass reflectors							
Spots	Microscope image	K_0_25	K_0_40	K_0_50	K_0.2_40	K_1_25	K_1_40	K_1_50	K_2_40
		--	--	--					
		0	0	0	6	8	8	12	95
Cut edges	Microscope image	--	--	--	264	706	597	1167	1188
		No corrosion	No corrosion	No corrosion	793	1095	1313	3981	cm order
Original edges	Microscope image								
		No corrosion	No corrosion	No corrosion	No corrosion	999	1081	3817	8959
		No corrosion	No corrosion	No corrosion	No corrosion	999	1081	3817	8959
Representative reflector samples	Photo (10x10) cm ² sample								
		$\Delta\rho_{\lambda,\varphi}$ (-)	0.000±0.000	0.000±0.000	-0.002±0.000	0.000±0.001	0.001±0.002	0.000±0.001	-0.002±0.002
		Total Corr. (%)	0.0±0.0	0.0±0.0	0.0±0.0	1.8±0.5	2.6±0.4	3.7±1.1	5.6±1.0
									11.5±1.6

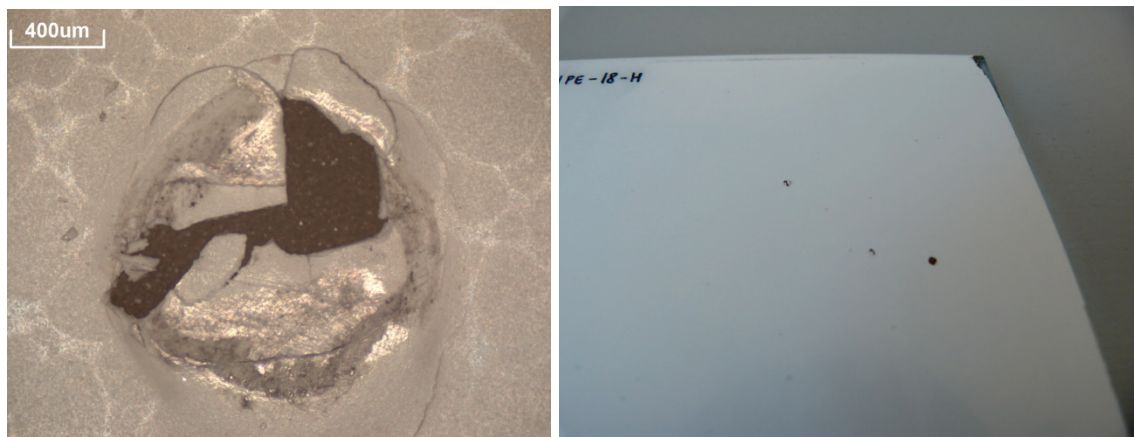

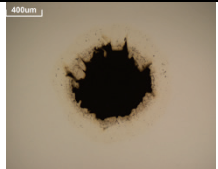
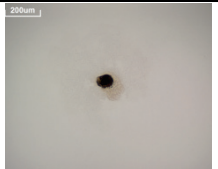





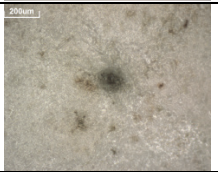



Fig. 4. Microscope image of a paint blister on the back of a Type 1 silvered-glass reflector sample taken at 5x magnification after 20 cycles of the K_0_40 humidity test (left), un magnified image of blisters (right).

Table 4

Microscope images of corrosion spots found on the reflective layer and corresponding pinholes in the paint on the back of Type 1 silvered-glass reflectors after 20 Kesternich test cycles. All images are 10x, except for Test K_1_25, which are 5x.

Defects	Type 1 silvered-glass reflectors				
	K 0.2 40	K 1 25	K 1 40	K 1 50	K 2 40
Spots					
Pinholes					

More detailed characterization was done on the reflective area near the scratch, which was expected to be the most sensitive part of the reflectors. First, monochromatic specular reflectance results are plotted over the number of Kesternich cycles in Fig. 5, showing that the tests without gas did not cause any significant change in this parameter. However, all the aging conditions with SO₂ show a similar downward trend up to a maximum decrease of -0.097±0.015, -0.093±0.014, -0.081±0.012 and -0.115±0.004 for the Tests K_0.2_40, K_1_25, K_1_40 and K_2_40, respectively. Test K_1_50 caused the greatest fall in specular reflectance (up to -0.214±0.032 after 20 cycles).

These significant reductions in reflectance were also corroborated by microscopic examination of the scratch. As may be seen in Table 5, the mean increment in scratch width (ΔW) is higher at the end of the tests with the most decrease in reflectance, which also show more corrosion. Again, the increment in scratch width (between 1200 and 1600 µm) is similar in Tests K_0.2_40, K_1_25, K_1_40 and K_2_40. On the contrary, in Test K_1_50, the scratch is so corroded that it is complicated to measure its width properly at the same magnification, as it increased by over 2000 µm. The maximum increase in width in the SO₂-free humidity tests is at least one order of magnitude lower than their counterparts in the Kesternich tests. The evolution of the mean increment in scratch width (in µm) in the tests is shown over the number of cycles in Fig. 6. Agreement between these results and the evolution of monochromatic specular reflectance shown in Fig. 5 is very good.

As shown in these figures, the weathering tests were classified as very low corrosion (K_0_25, K_0_40 and K_0_50), medium corrosion (K_0.2_40, K_1_25, K_1_40 and K_2_40) and high corrosion (K_1_50). Nevertheless, taking into account the corrosion features in the rest of the reflector area (Table 3), Tests K_0.2_40 and K_2_40 may be regarded as low and high, respectively. Therefore, although the corrosion severity of the tests without SO₂ is very low, and becomes more significant as the testing temperature rises, in the experiments with gas, the corrosion is much stronger, especially at high *T* and gas concentrations.

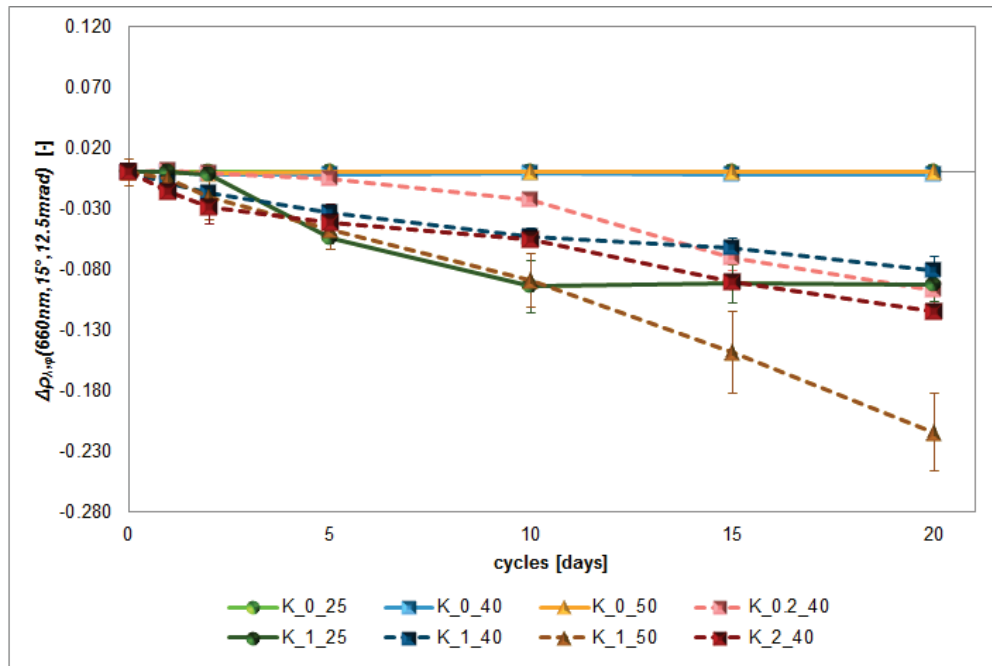
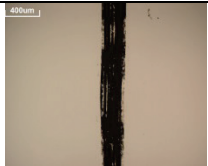
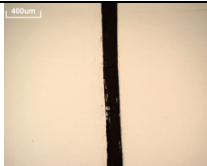




Fig. 5. Evolution over 24-hour cycles of the mean increment in monochromatic specular reflectance measured in the area of the scratch in Type 1 silvered-glass reflectors in the weathering tests.

Table 5

Summary of corrosion found in the area near the scratch on Type 1 silvered-glass reflectors after 20 aging cycles in all tests. ΔW : mean increment in scratch width (μm), $\Delta\rho_{\lambda,\varphi}$: mean increment in monochromatic specular reflectance in the scratch (-). All microscope images are 5x.

Scratches on Type 1 silvered-glass reflectors				
Test	K_0_25	K_0_40	K_0_50	K_0.2_40
Microscope image				
ΔW (μm)	+91.5 \pm 0.0	+153.7 \pm 0.0	+108.9 \pm 0.0	+1207.2 \pm 93.9
$\Delta\rho_{\lambda,\varphi}$ (-)	0.000 \pm 0.000	-0.002 \pm 0.001	0.001 \pm 0.000	-0.097 \pm 0.015
Test	K_1_25	K_1_40	K_1_50	K_2_40

Microscope image				
ΔW (μm)	+1411.7 \pm 719.8	+1465.6 \pm 173.3	+2007.1 \pm 224.8	+1571.6 \pm 165.1
$\Delta\rho_{\lambda,\varphi}$ (-)	-0.093 \pm 0.014	-0.081 \pm 0.012	-0.214 \pm 0.032	-0.115 \pm 0.004

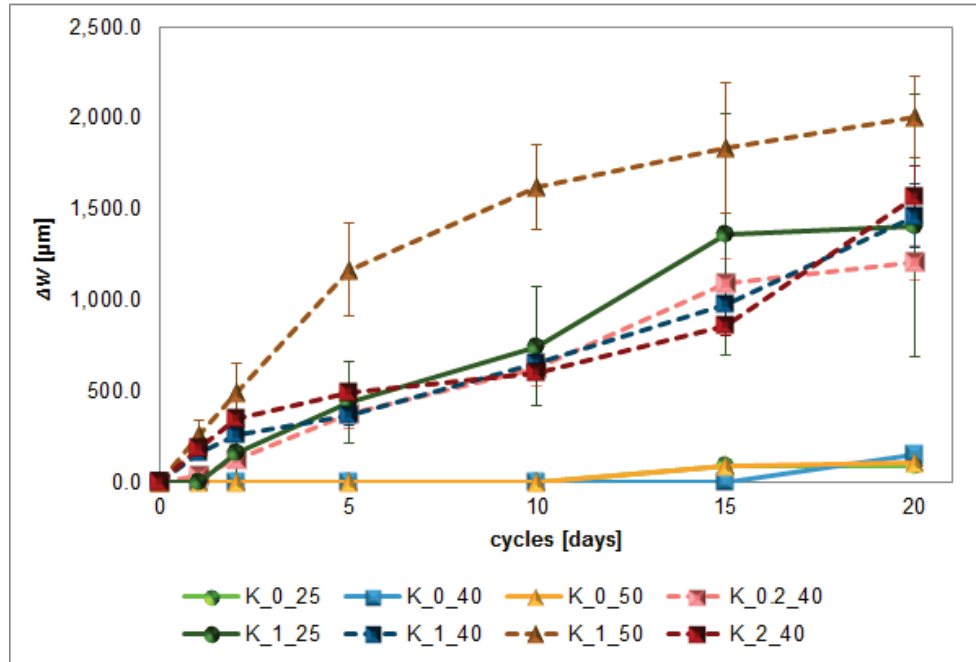


Fig. 6. Evolution of the mean scratch width increment (μm) on Type 1 silvered-glass reflectors during cycles in the different corrosion tests.

3.2. Undamaged silvered-glass reflectors (Type 2)

As in the first reflector material studied, monochromatic specular and hemispherical reflectance was also measured on the whole undamaged reflective area of Type 2 silvered-glass reflectors, as plotted over the number of cycles in Figs. 7left and right. No decrease in reflectance was observed after the humidity tests without gas, except for Test K_0_50, which was responsible for a loss of -0.006 ± 0.000 in specular reflectance. There was no significant reduction in reflectance either in K_0_2_40, K_1_25 or K_1_40 (classified as low and medium corrosion tests for Type 1 silvered-glass reflectors). However, the K_1_50 and K_2_40 high corrosion tests did cause a major decrease in both specular and hemispherical reflectance, especially after 20 cycles of Test K_2_40, in which there was a loss of -0.635 ± 0.153 in specular reflectance. Such strong reductions in reflectance of previously undamaged silvered-glass reflectors have not been reported for accelerated aging tests with corrosive gas [31]. Therefore, the Kesternich test can be regarded as a very aggressive corrosion test for silvered-glass reflectors, especially when extreme conditions of gas concentration or temperature are selected.

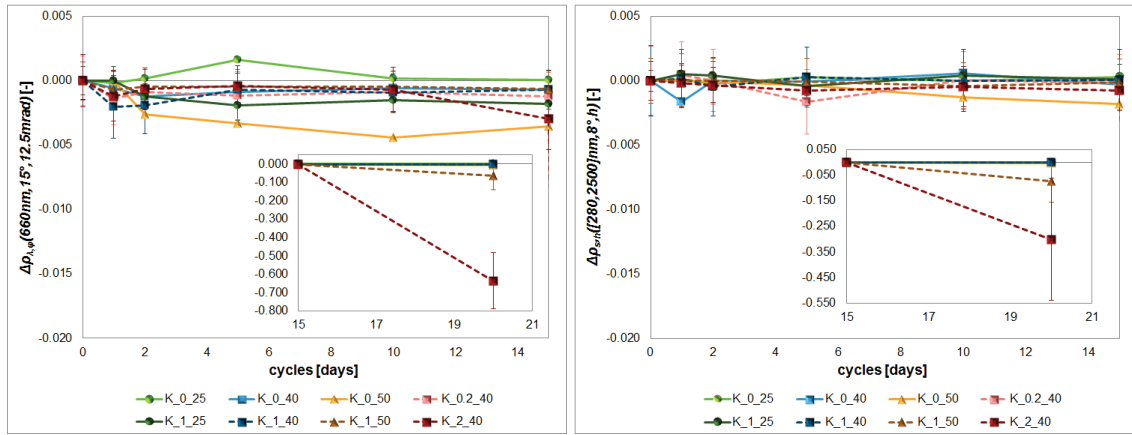


Fig. 7. Mean increment in monochromatic specular reflectance (left) and in solar-weighted hemispherical reflectance (right) over the whole reflective area of Type 2 silvered-glass reflectors during weathering test cycles.

The reflectance results were confirmed by microscopic examination. Table 6 summarizes the most important corrosion defects found on the reflective layer of Type 2 silvered-glass reflectors at the end of testing (20 cycles). It may be seen that K_0.2_40, K_1_25 and K_1_40 caused similar corrosion on the reflective layers with total corroded areas of $(0.7 \pm 0.1)\%$, $(1.5 \pm 0.3)\%$ and $(1.0 \pm 0.2)\%$, respectively. However, after K_1_50, abundant corrosion spots (67) appeared, more corrosion developed near the original edges (almost 1 mm) and $(2.5 \pm 1.4)\%$ of total corrosion. Finally, the most dramatic changes were found after the test with the highest SO_2 concentration (K_2_40). The many (370) large spots that appear on the reflective area of the specimens and the extreme mean size of the corroded area, $(35.8 \pm 5.3)\%$, provide good evidence of its highly corrosive character, as shown by the optical microscope images and the picture of the whole sample in Table 6. Finally, the tests without gas barely generated any corrosion on the samples, but did cause the formation of a significant number of blisters on the painted side of the reflectors (see Fig. 8). As discussed above for Type 1 silvered-glass reflectors, these blisters may evolve into pinholes when SO_2 gas is added to the test environment. Several corrosion spots and their corresponding pinholes in the paint on the back of the reflector are displayed in Table 7.

Table 6

Summary of corrosion found on the reflective area of Type 2 silvered-glass reflectors after 20 cycles of all weathering tests. Total N : sum of the number of corrosion spots visible to the naked eye at the end of testing on a 300-cm^2 total reflector surface, Size: characteristic length of the largest spot (μm), Max. Pen.: maximum penetration of corrosion near the edge (μm), $\Delta\rho_{\lambda,\varphi}$: mean increment in monochromatic specular reflectance on the whole reflector surface (-), Total Corr.: mean total corrosion of the whole reflector surface (%). 5x microscope images of the spots and 10x of original edges.

Corrosion features		Reflective area of Type 2 silvered-glass reflectors							
		K_0_25	K_0_40	K_0_50	K_0.2_40	K_1_25	K_1_40	K_1_50	K_2_40
Spots	Image	--	--	--					
	Total <i>N</i>	0	0	0	26	28	29	67	370
	Size (μm)	--	--	--	1092	1251	1112	1002	2339
Original edges	Image								
	Max. Pen. (μm)	No corrosion	No corrosion	No corrosion	500	901	788	937	cm order
Representative reflector samples	Photo (10x10) cm ² sample								
	$\Delta\rho_{\text{L},0}$ (-)	0.000±0.000	-0.001±0.000	-0.006±0.000	-0.001±0.002	-0.002±0.001	-0.001±0.001	-0.064±0.076	-0.635±0.153
	Total Corr. (‰)	0.0±0.0	0.0±0.0	0.0±0.0	0.7±0.1	1.5±0.3	1.0±0.2	2.5±1.4	35.8±5.3

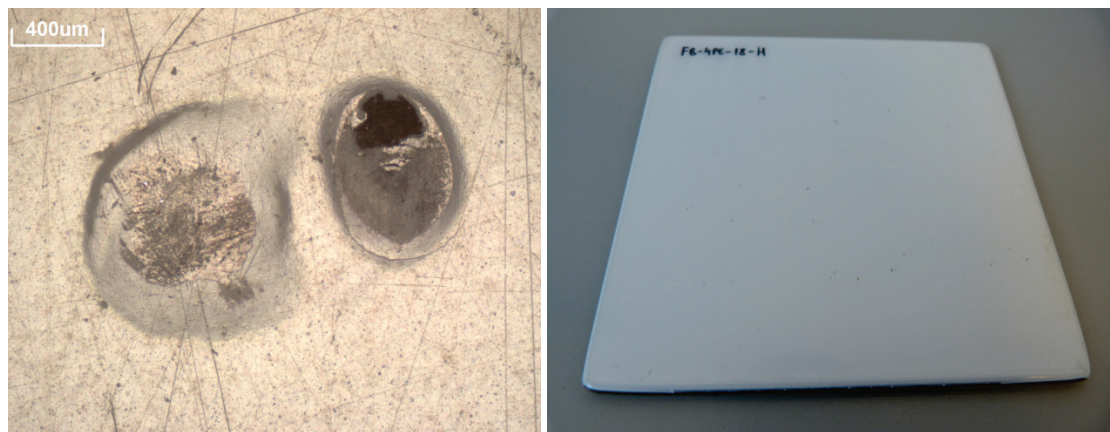
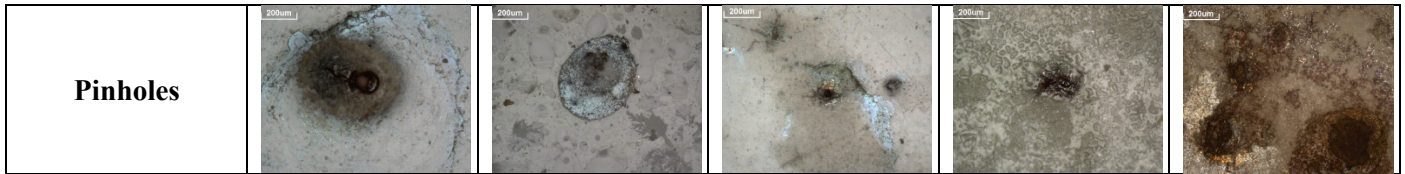


Fig. 8. 5x microscope image of blisters found in the paint on the back of a Type 2 silvered-glass reflector sample after 20 cycles of the K_0_40 humidity test (left), picture of the appearance of blisters at naked eye (right).

Table 7

10x microscope images of corrosion spots found on the reflective layer and corresponding pinholes in the paint on the back of Type 2 silvered-glass reflectors after 20 Kesternich test cycles.

Defects	Type 2 silvered glass reflectors				
	K_0.2_40	K_1_25	K_1_40	K_1_50	K_2_40
Spots					



Summarizing, while the tests with low and moderate gas concentration and temperature conditions (K_0_2_40, K_1_25 and K_1_40) were responsible for moderate degradation of samples, the tests with the highest $[SO_2]$ or T , i.e. Tests K_1_50 and K_2_40, led to massive corrosion, both on the reflective and painted layers of the undamaged silvered-glass reflectors. However, the humidity tests without gas (K_0_25, K_0_40 and K_0_50) did not significantly alter their properties. SO_2 corrosion defects were the same sort as in the studies of predamaged silvered-glass reflectors, and the general conclusions drawn are also similar. Comparing the percentage of total area corroded on both reflector types (see Tables 3 and 6), degradation of the undamaged materials at the end of every test was less than on the predamaged ones, except for the most aggressive test (K_2_40). This is because Type 2 reflectors have larger corrosion spots and more of them than Type 1 in most tests, whereas in the latter, both cut and original edges were in poorer condition. The results also suggest stronger influence of the high SO_2 concentration than temperature in silvered-glass reflector degradation. Moreover, it is important to highlight that the two types of reflectors were fabricated by the same manufacturer and had the same reflective and paint-layer structure, but Type 1 reflectors were industrial, whereas Type 2 were manufactured to order on a small scale. These findings therefore show the strong influence of material processing on the final properties of reflectors. Thus subtle differences in layer composition (due to different amounts of impurities) or structure (grain size, porosity, film homogeneity or thickness, etc.) may be responsible for the significantly higher corrosion observed at high SO_2 concentrations in Type 2 reflectors than in Type 1.

3.3. Predamaged aluminum reflectors (Type 3)

The third type of solar reflector was studied following a procedure similar to those above. First, monochromatic specular and hemispherical reflectance on the undamaged reflective area of samples was monitored during the tests. Results are shown in Fig. 9, where the greatest decrease in specular reflectance (-0.008 ± 0.016) was found after Test K_2_40 (Fig. 9left). No significant reduction in reflectance was detected in the rest of tests, although there was an anomalous loss of -0.006 ± 0.000 in specular reflectance within the range of experimental errors for the test at 40 °C without gas (K_0_40). There was no significant decrease in solar-weighted hemispherical reflectance as shown in Fig. 9right.

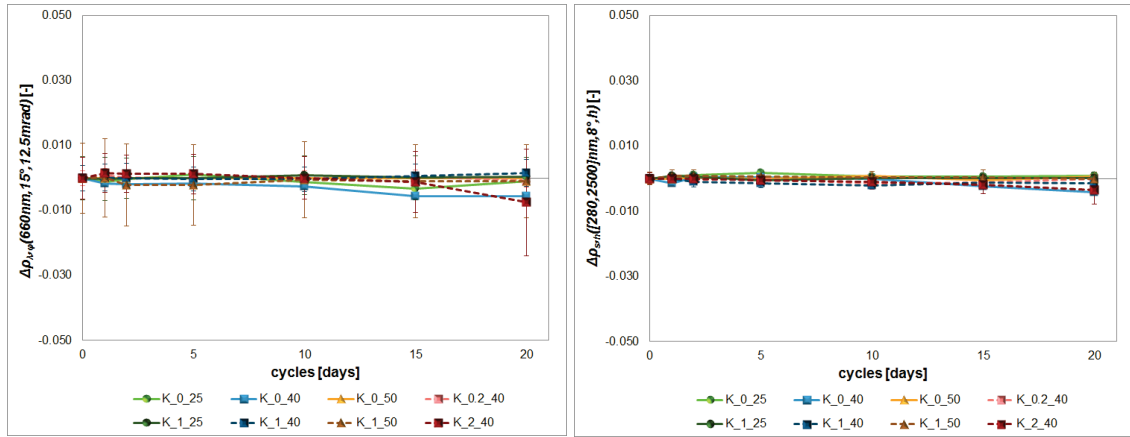

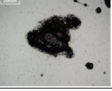
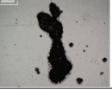
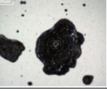
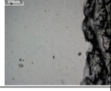

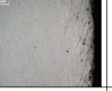
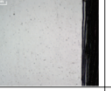
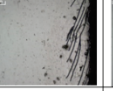
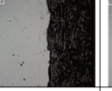


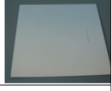

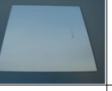
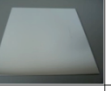

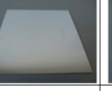
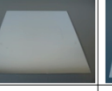



Fig. 9. Evolution of the mean increment in monochromatic specular reflectance (left) and solar-weighted hemispherical reflectance (right) during weathering test cycles on the originally undamaged areas of aluminum reflectors.

Table 8 is an overview of the most significant corrosion features found on the reflective layer of aluminum reflectors at the end of testing. As previously pointed out, optical microscope results provide a more detailed view of the real state of corrosion than the reflectance data. There was no change in the microscopic features of samples after the humidity tests (K_0_25, K_0_40, K_0_50) or the low corrosion test (K_0.2_40). However, visible black spots appeared on the reflective surface of materials after the medium (K_1_25, K_1_40) and high (K_1_50, K_2_40) corrosion tests. Bare edges thickened noticeably. The most harmful test was K_2_40, as demonstrated by the total number of corrosion spots (681) and the general appearance of the reflector surface. Therefore, test aggressiveness for aluminum reflectors observed under the microscope is in general agreement with what was found for the reflector types discussed above.

Table 8

Summary of corrosion found on the reflective area of the aluminum reflectors after 20 cycles of all weathering tests. Total N : sum of the number of corrosion spots visible to the naked eye at the end of testing on a 300-cm² total reflector surface, Size: characteristic length of the largest spot (μm), Max. Pen.: maximum penetration of corrosion near the edge (μm), $\Delta\rho_{\lambda,\phi}$: mean increment in monochromatic specular reflectance on reflector surfaces not predamaged (-), Total Corr.: mean total corrosion of the whole reflector surface (%). Microscope images are 10x.

Corrosion features		Reflective area of aluminum reflectors							
		K_0_25	K_0_40	K_0_50	K_0.2_40	K_1_25	K_1_40	K_1_50	K_2_40
Spots	Image	--	--	--	--				
	Total N	0	0	0	0	47	100	225	681
	Size (μm)	--	--	--	--	505	590	854	760
Original edges	Image								
	Max. Pen. (μm)	No corrosion	No corrosion	No corrosion	91	251	437	574	437
Representative reflector samples	Photo (12x12) cm^2 sample								
	$\Delta\rho_{\lambda,0}$ (-)	-0.001 \pm 0.000	-0.006 \pm 0.000	0.000 \pm 0.000	-0.001 \pm 0.002	0.000 \pm 0.006	0.002 \pm 0.004	-0.001 \pm 0.011	-0.008 \pm 0.016
	Total Corr. ($^\circ\text{e}$)	0.0 \pm 0.0	0.0 \pm 0.0	0.0 \pm 0.0	1.3 \pm 0.2	1.9 \pm 0.5	3.8 \pm 0.2	3.8 \pm 0.5	5.1 \pm 1.1

Several parameters of the scratch were analyzed in more detail, the same as for Type 1 silvered-glass reflectors. Thus, monochromatic specular reflectance was measured in the area of the scratch during the tests as shown in Fig. 10. Whereas Tests K_0_25, K_0_40, K_0_50, K_0.2_40, K_1_25 and K_1_40 did not modify reflectance, K_1_50 and K_2_40 were responsible for monochromatic specular reflectance reductions of -0.005 ± 0.012 and -0.013 ± 0.014 in the scratch, respectively. The severity of the high corrosion tests is also confirmed by microscopic measurements of the scratch width (see Table 9 and Fig. 11). The largest changes in scratch width were found after K_2_40 and K_1_50, followed by K_1_40 and K_0.2_40. However, no significant modifications in scratch width were observed after the rest of the tests, even those without gas and the K_1_25 test, in spite of the spots that were observed at the end of this ambient temperature test with a medium SO_2 concentration (see Table 9).

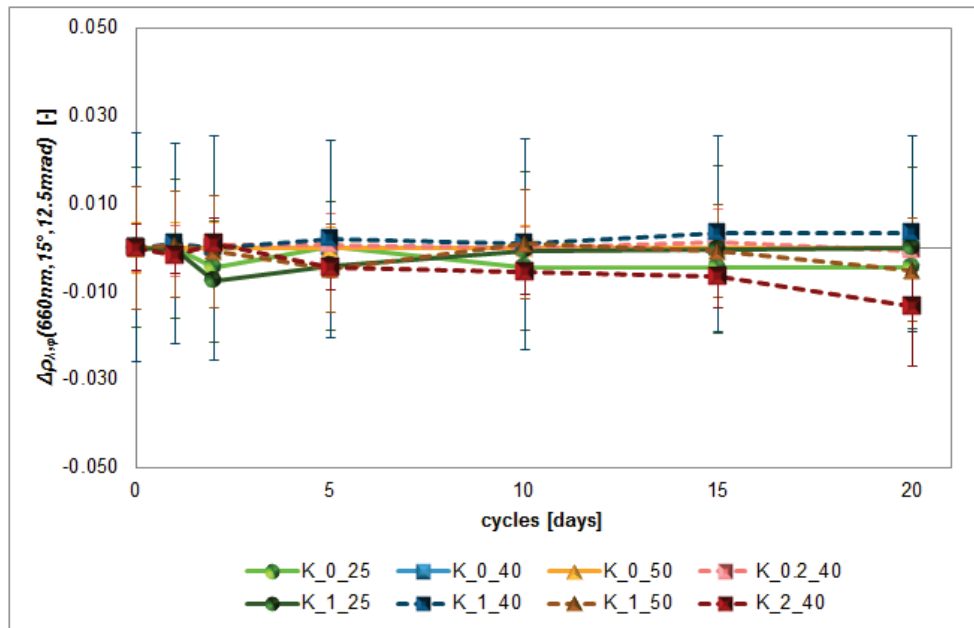
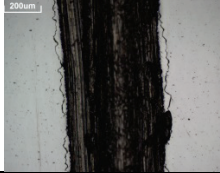
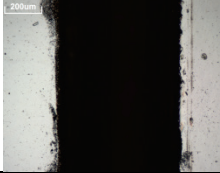
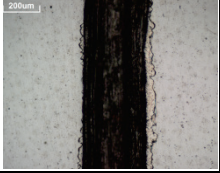
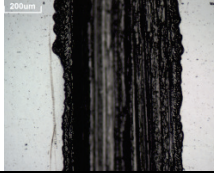
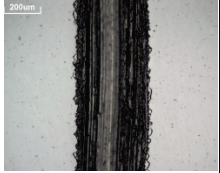
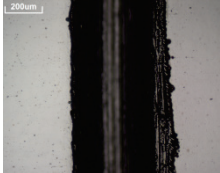
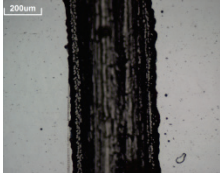
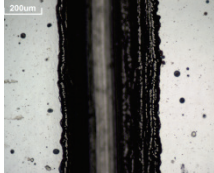


Fig. 10. Evolution of the mean increment in monochromatic specular reflectance over 24-hour cycles measured in the area of the scratch on aluminum reflectors in the weathering tests.

Table 9

Summary of corrosion found in the area near the scratch on aluminum reflectors after 20 aging cycles in all tests. ΔW : mean increment in scratch width (μm), $\Delta\rho_{\lambda,\varphi}$: mean increment in monochromatic specular reflectance in the scratch (-). All microscope images are 10x.

Scratches on aluminum reflectors				
Test	K_0_25	K_0_40	K_0_50	K_0.2_40
Microscope image				
ΔW (μm)	0.0 \pm 0.0	0.0 \pm 0.0	+0.9 \pm 0.0	+20.7 \pm 18.5
$\Delta\rho_{\lambda,\varphi}$ (-)	-0.001 \pm 0.001	-0.001 \pm 0.000	0.000 \pm 0.000	-0.001 \pm 0.004
Test	K_1_25	K_1_40	K_1_50	K_2_40
Microscope image				
ΔW (μm)	0.0 \pm 0.0	+22.3 \pm 28.7	+38.4 \pm 25.8	+39.4 \pm 28.8
$\Delta\rho_{\lambda,\varphi}$ (-)	0.000 \pm 0.018	0.003 \pm 0.022	-0.005 \pm 0.012	-0.013 \pm 0.014

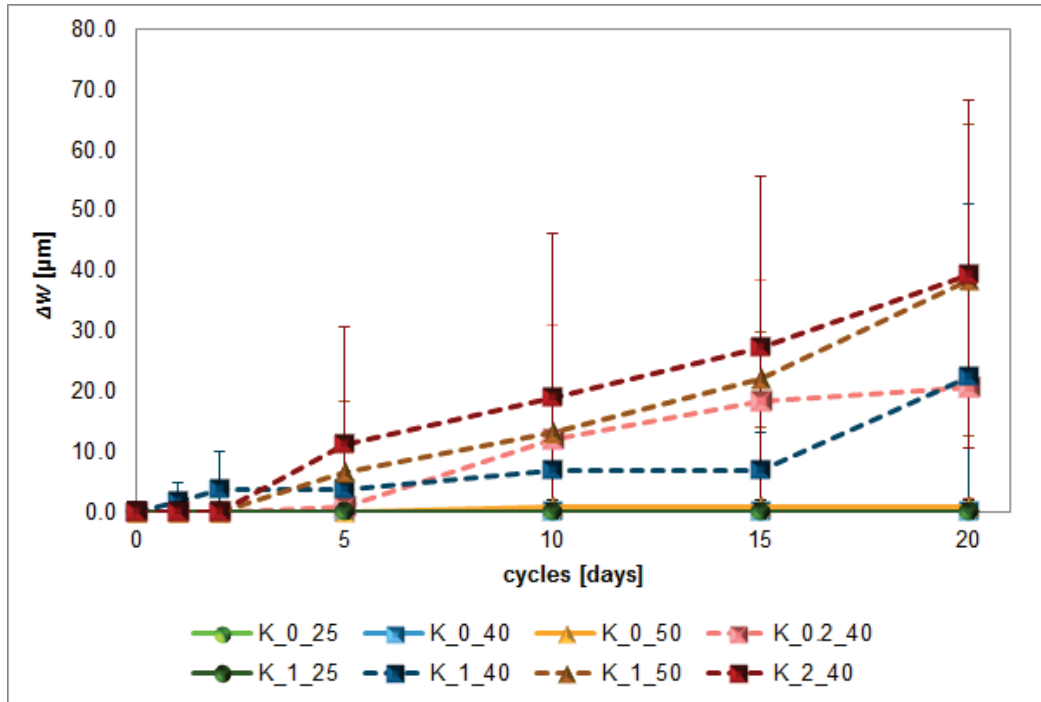


Fig. 11. Evolution of the mean increment in scratch width (μm) in aluminum reflectors over corrosion test cycles.

Summarizing, aluminum reflectors were generally not as corroded by the Kesternich tests as silvered-glass reflectors. As reported in previous studies, degradation of aluminum reflectors is rather slow, mostly because of their protective SiO_2 layer [23], and entails various factors including moisture, abrasion and pollutants during long exposure [13]. In this study, only the two extreme tests (K_2_40, with the highest SO_2 concentration, and K_1_50, with the highest temperature) caused any corrosion detectable under the microscope, but it was harder to detect by monochromatic specular reflectance. In light of these results, both the corrosive gas concentration and its synergism with temperature and humidity are key factors to be considered in aluminum reflector durability studies, as the most corrosion was found in the test with the highest gas concentration and intermediate temperature (K_2_40).

3.4. Comparisons with real outdoor data

The most informative and aggressive test (K_2_40) was compared to real data from corroded mirror facets at a commercial CSP plant near an industrial site[†]. After three years of exposure at this site, the PTC facets were inspected, and a mean pitting corrosion area of 0.16% was estimated. Both the Type 1 silvered-glass reflectors and the samples from this commercial CSP plant were from industrial PTC facets made by the same manufacturer and have the same layered structure. Indeed, corrosion spots found on Type 1 silvered-glass reflectors were very similar to the on-site facets, as shown in Fig. 12. Type 2 silvered-glass reflectors, however, although by the same manufacturer, were specifically manufactured at small scale in a $10 \times 10 \text{ cm}^2$ format, and hence, these results are not comparable.

[†] The exact location cannot be revealed due to [confidentiality of information](#)

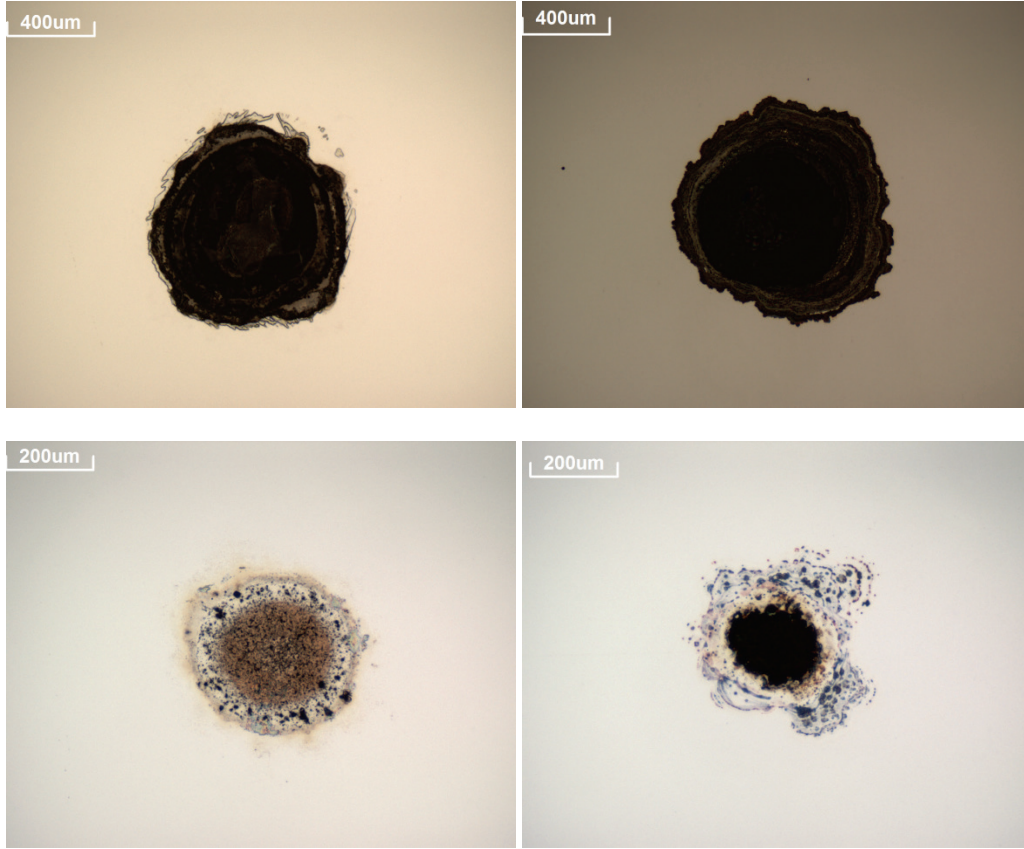


Fig. 12. Microscope images of corrosion spots on Type 1 silvered-glass reflectors in on-site PTC facets after 20 cycles of Test K_2_40 (left) and after three years at a commercial CSP plant near an industrial site (right).

The growth of corrosion spots on Type 1 silvered-glass reflectors was monitored during the K_2_40 test cycles by microscopic measurement. Thus, the areas of representative spots could be calculated, and by combining them with the total number of spots, the mean corroded area (per three specimens during the test cycles) was arrived at. Fig. 13 shows the mean area of corrosion spots (%) on Type 1 silvered-glass reflectors over the number of test cycles. The measurements are marked with orange circles and the solid line is the best fit found with a determination coefficient of 0.9997, which corresponds to an exponential function as shown in Eq. (1):

$$y = 7 \cdot 10^{-5} \exp[0.4048x] \quad (1)$$

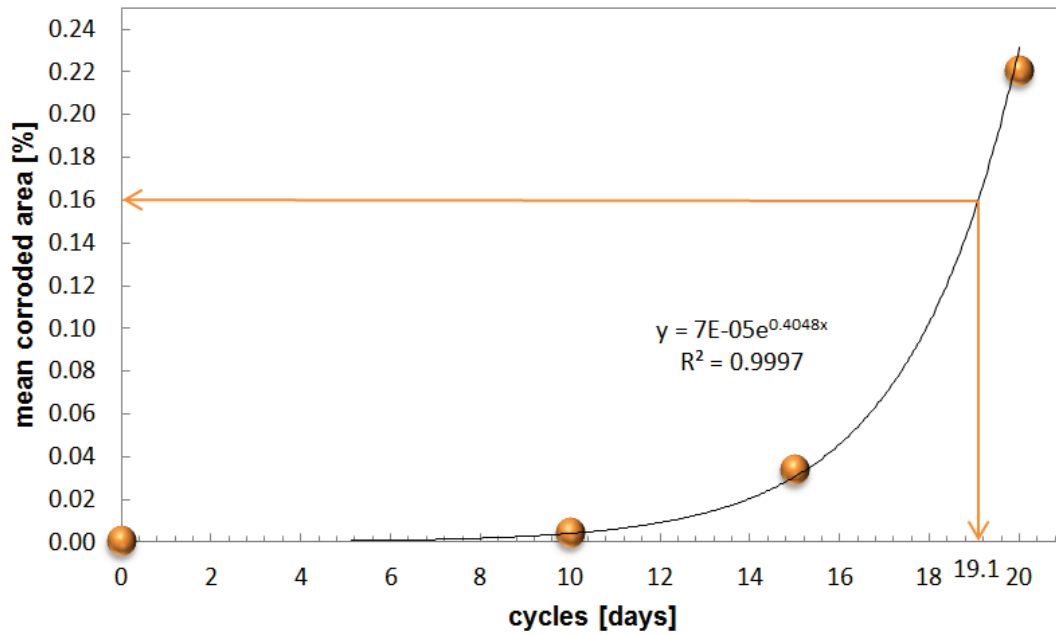


Fig. 13. Growth of mean area of corrosion spots (%) on Type 1 silvered-glass reflectors during K_2_40 test cycles.

This correlation enabled the K_2_40 test time (24-hour cycles) equivalent to real on-site degradation to be found, i.e. 0.16% after 19.1 test cycles (458 h), as marked with orange arrows in Fig. 13. As the real exposure time was three years, the acceleration factor would be 57 for the study exposure site. These rough calculations, which are a first step in the correlation of accelerated tests with real outdoor exposures, may be very valuable, since such estimates for commercial CSP silvered-glass reflectors are rarely found in the literature.

4. Conclusions

Solar reflectors for CSP applications were subjected to humid atmospheres containing SO₂ in accelerated aging tests simulating aggressive industrial environments. Based on Kesternich test methods, three types of commercial reflector materials were weathered in water-saturated SO₂ atmospheres at several temperatures and concentrations and with no SO₂. The tests were monitored by reflectance measurements and by examination under optical microscope. Predamaged silvered-glass reflectors (Type 1) showed no significant reduction in reflectance on originally undamaged areas. However, microscopic inspection revealed major degradation of both the whole surface and scratch after the most aggressive tests (1.0 dm³ SO₂ at 50°C, K_1_50; and 2.0 dm³ SO₂ at 40°C, K_2_40), the test at the highest gas concentration being more harmful than the one at the highest temperature. Corrosion spots appeared on the reflective silver layer and blisters that could turn into pinholes on the painted protective back layer, which were most noticeable in the SO₂-free tests. The presence of a pinhole often triggers the formation of a corrosion spot. Therefore, the extreme K_2_40 test should be selected for significant results in a short time, although Test K_1_50 may be considered suitable for Type1

silvered-glass reflectors, because it also gives representative results with a lower concentration of SO₂, and is therefore more cost-effective and less environmentally hazardous.

Undamaged silvered-glass reflectors (Type 2), on the other hand, generally exhibited poorer performance than Type 1 reflectors. Although the latter had more corroded edges, Type 2 reflectors not only showed more, larger corrosion spots in most tests, but also underwent high specular reflectance losses of up to -0.635 ± 0.153 at the end of the K_2_40 test. Small-size samples of this reflector type were specially manufactured at small scale and did not come from real PTC mirror facets as did the Type 1 reflector samples. Therefore, Kesternich tests at high gas concentrations or temperatures are considered too extreme, and more moderate conditions such as the K_1_40 test are recommended for more realistic Type 2 reflector results.

Finally, Type 3 predamaged aluminum reflectors were not as corroded as silvered-glass reflectors, but they underwent visible degradation, mainly as black spots on the reflective surface and scratch. Again, Test K_2_40 was the most corrosive due to its high SO₂ concentration, but synergies with temperature and humidity are key factors that must be considered as well. Therefore, the K_2_40 test is recommended for aluminum reflectors. For low-concentrating systems where specularity is not the limiting factor (such as small PTCs for process heat applications) aluminum reflectors would be worthwhile because they can withstand highly corrosive acid atmospheres better than silvered-glass reflectors.

In addition, results from Test K_2_40 were compared to corrosion data from real on-site PTC facets located near an industrial environment. Microscopic defects found in Type 1 silvered-glass reflectors were very similar to corrosion spots in the on-site facets. An estimated acceleration factor of 57 correlates Test K_2_40 with this real outdoor exposure affected by a highly polluted industrial atmosphere. This may be considered a valuable contribution to the service lifetime prediction of solar reflector materials, especially the widely deployed silvered-glass reflectors.

The immediate implications of this study are its relevance to research in the effects of acid rain environments on other CSP components, such as PTC absorber tubes or open volumetric receivers in solar towers. Apart from the diversification of accelerating aging tests, this study aimed to highlight the importance of proper CSP facility siting, avoiding areas with highly polluted atmospheres near industrial sites if possible.

Acknowledgments

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